

# Fusion and industrial plasma technologies

## L7: Industrial plasmas 2

H. Reimerdes

Based on lecture notes by A. Howling

1. Introduction to basic industrial plasmas
  - Plasma medicine
2. Breakdown and Paschen's law
  - Communication satellite
3. Sheath and plasma etching
  - Microelectronics
4. Plasma with insulating electrodes
  - Large area displays/solar cells



L6

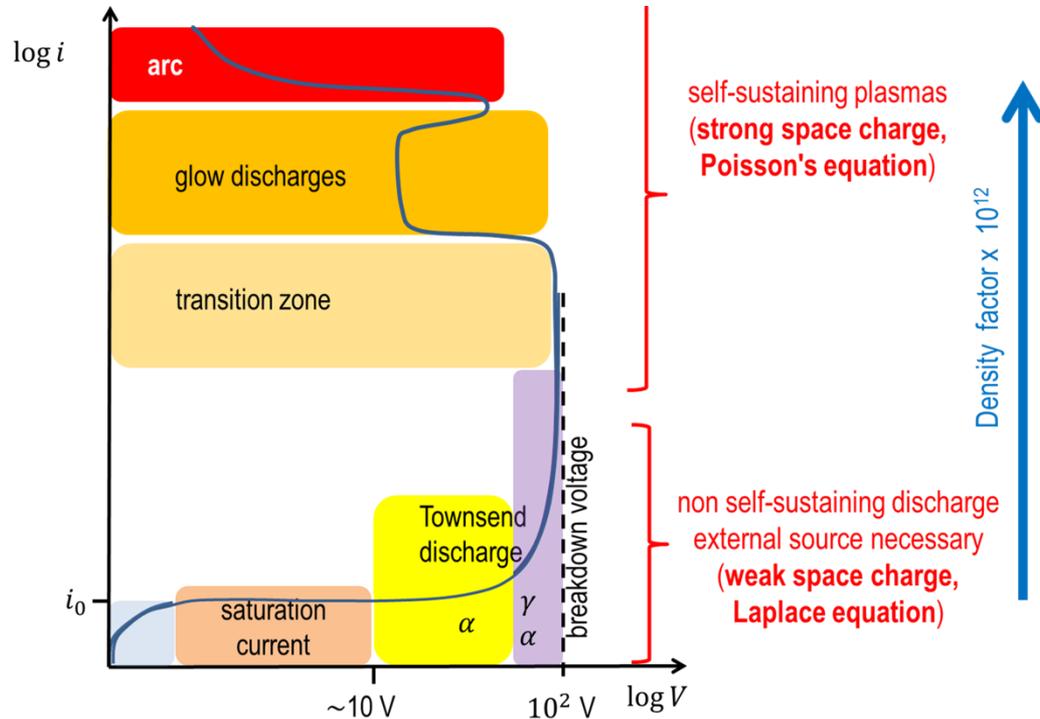
L7

## Material

- See also EPFL MOOC “Plasma physics: Applications” #5a-g
  - [https://courses.edx.org/courses/course-v1:EPFLx+PlasmaApplicationX+1T\\_2018](https://courses.edx.org/courses/course-v1:EPFLx+PlasmaApplicationX+1T_2018)
- M. Lieberman & A. Lichtenberg, “Principles of plasma discharges and materials processing”, Section 6.1-6.2

# Formation of a plasma

- Development from Townsend discharge to plasma glow and arc



## 1. Introduction to basic industrial plasmas

- Plasma medicine

## 2. Breakdown and Paschen's law

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## 3. Sheath and plasma etching

- Microelectronics

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- Large area displays/solar cells



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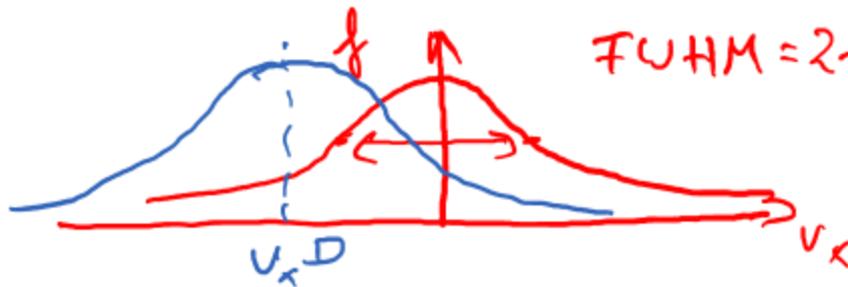
# Reminder: Maxwell-Boltzmann distribution

- Velocity distribution in an ideal gas in thermodynamic equilibrium

$$f_s(\vec{v}) = \left( \frac{m_s}{2\pi k_B T_s} \right)^{3/2} e^{-\frac{m_s \vec{v}^2}{2k_B T_s}}$$

Distribution of velocity in one direction

$$f_s(v_x) = \iint f_s(v_x, v_y, v_z) dv_y dv_z = \left( \frac{m}{2\pi kT} \right)^{0.5} e^{-\frac{mv_x^2}{2kT}} \quad \text{Gaussian with } \sigma^2 = \frac{kT}{m}$$



# Reminder: Maxwell-Boltzmann distribution

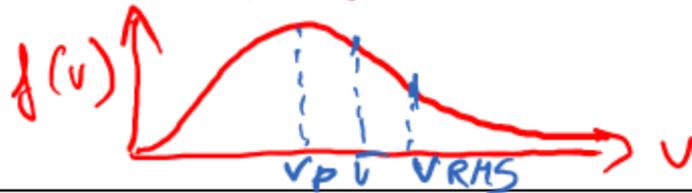
- Velocity distribution in an ideal gas in thermodynamic equilibrium

$$f_s(\vec{v}) = \left( \frac{m_s}{2\pi k_B T_s} \right)^{3/2} e^{-\frac{m_s \vec{v}^2}{2k_B T_s}}$$

Distribution of speed  $v = |\vec{v}|$

$$v = \sqrt{v_x^2 + v_y^2 + v_z^2} \quad ; \quad dv_x dv_y dv_z = v^2 dv d\Omega \quad \uparrow 4\pi$$

$$f(v) = \left( \frac{m}{2\pi k_B T} \right)^{3/2} 4\pi v^2 e^{-\frac{mv^2}{2k_B T}}$$



$$v_p = \sqrt{\frac{2k_B T}{m}}$$

$$\bar{v} = \sqrt{\frac{8k_B T}{\pi m}}$$

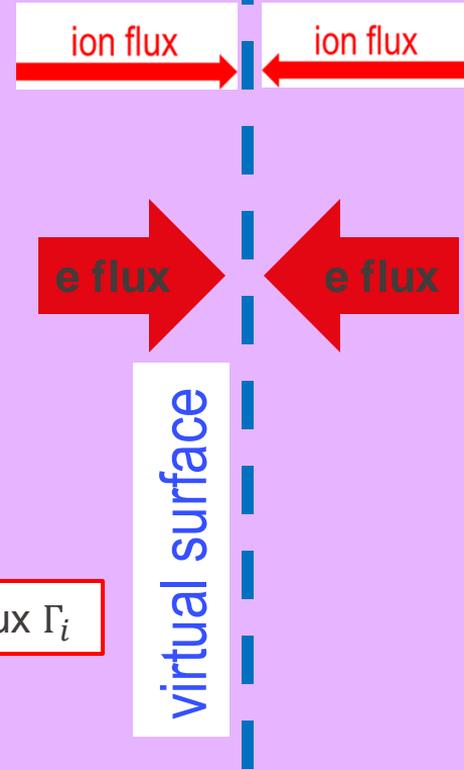
$$v_{\text{rms}} = \sqrt{\frac{3k_B T}{m}}$$

# Formation of a sheath

$$\text{Ion thermal flux } \Gamma_i = n_i \frac{\bar{v}_i}{4} = \frac{n_i}{4} \sqrt{\frac{8eT_i}{\pi m_i}}$$

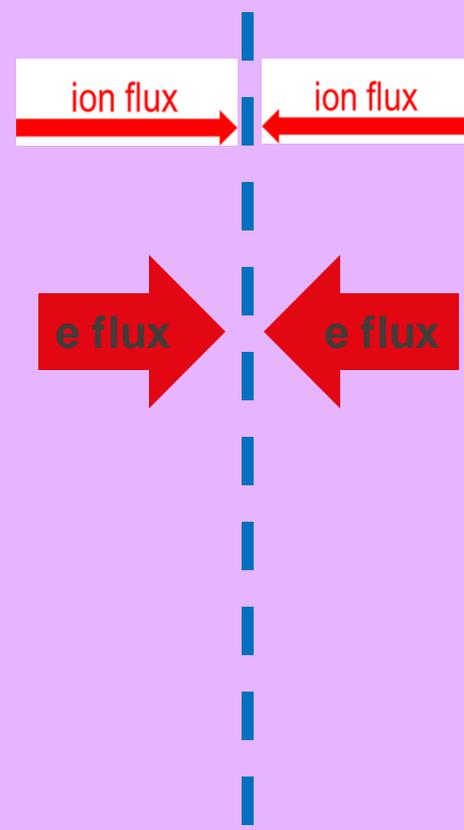
$$\text{Electron thermal flux } \Gamma_e = n_e \frac{\bar{v}_e}{4} = \frac{n_e}{4} \sqrt{\frac{8eT_e}{\pi m_e}}$$

Electron thermal flux  $\Gamma_e \gg$  Ion thermal flux  $\Gamma_i$



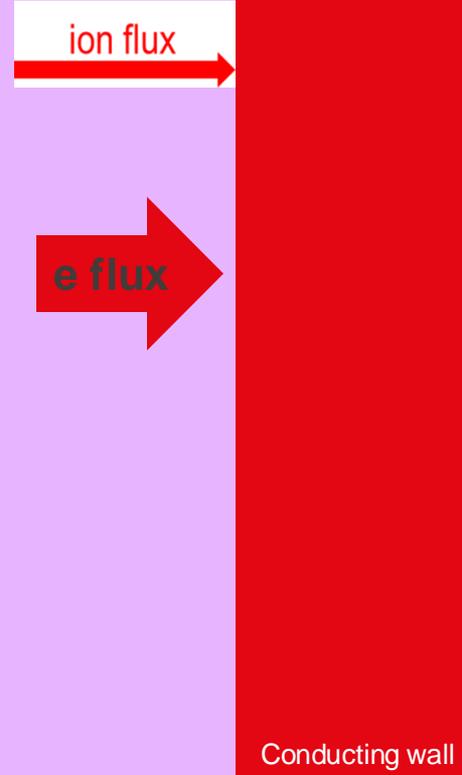
# Formation of a sheath

- So far, the plasma was always in isolation from its environment
- However, a plasma-wall interaction is unavoidable and necessary for plasma applications (deposition, etching, surface modifications, etc.)



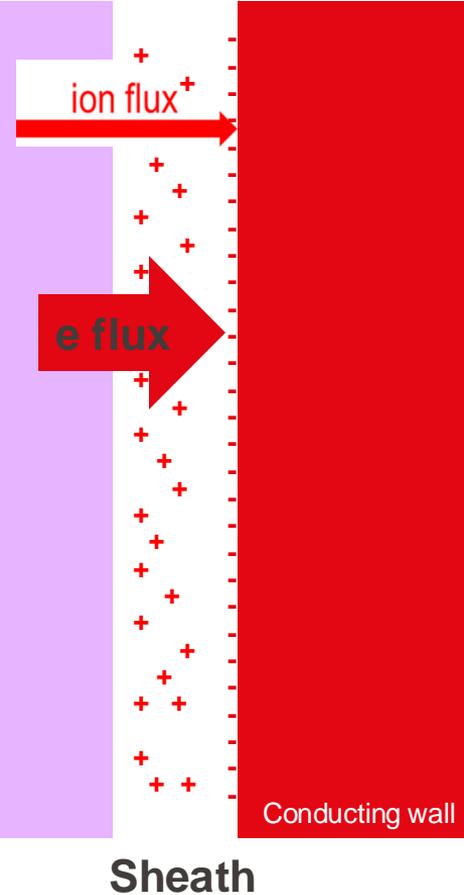
# Formation of a sheath

- What happens, if the virtual surface is replaced with a conducting wall?



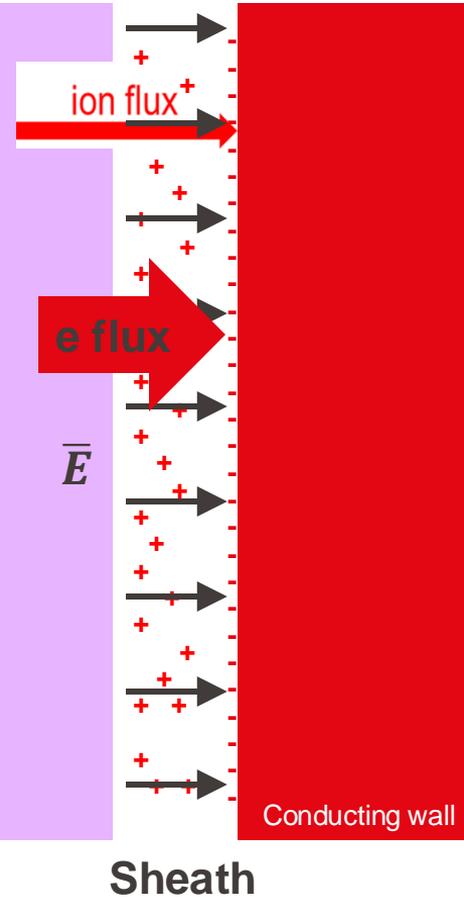
# Formation of a sheath

- Fast electrons rush to the wall, leaving behind a layer of slower ions



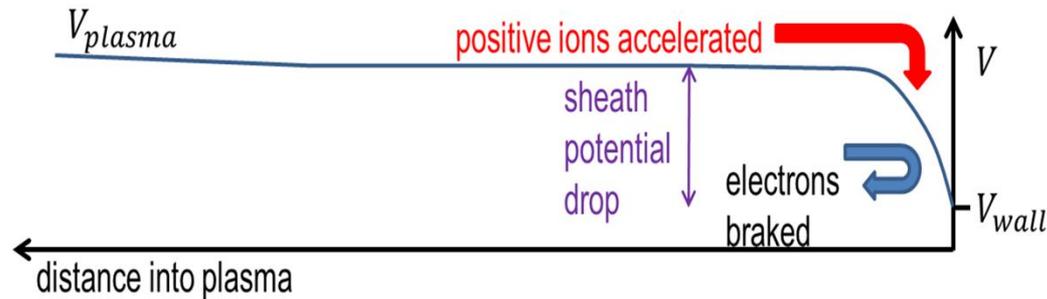
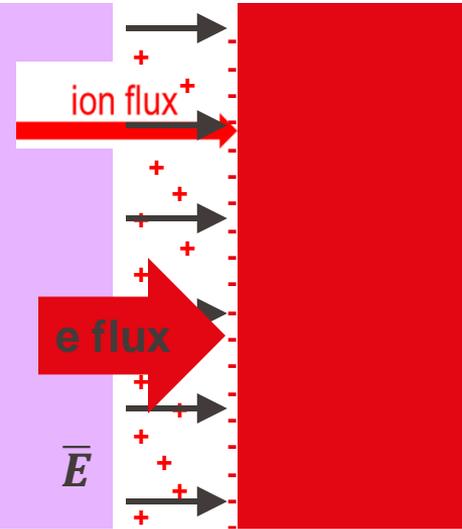
# Formation of a sheath

- Fast electrons rush to the wall, leaving behind a layer of slower ions
- Plasma potential increases until fluxes become equal



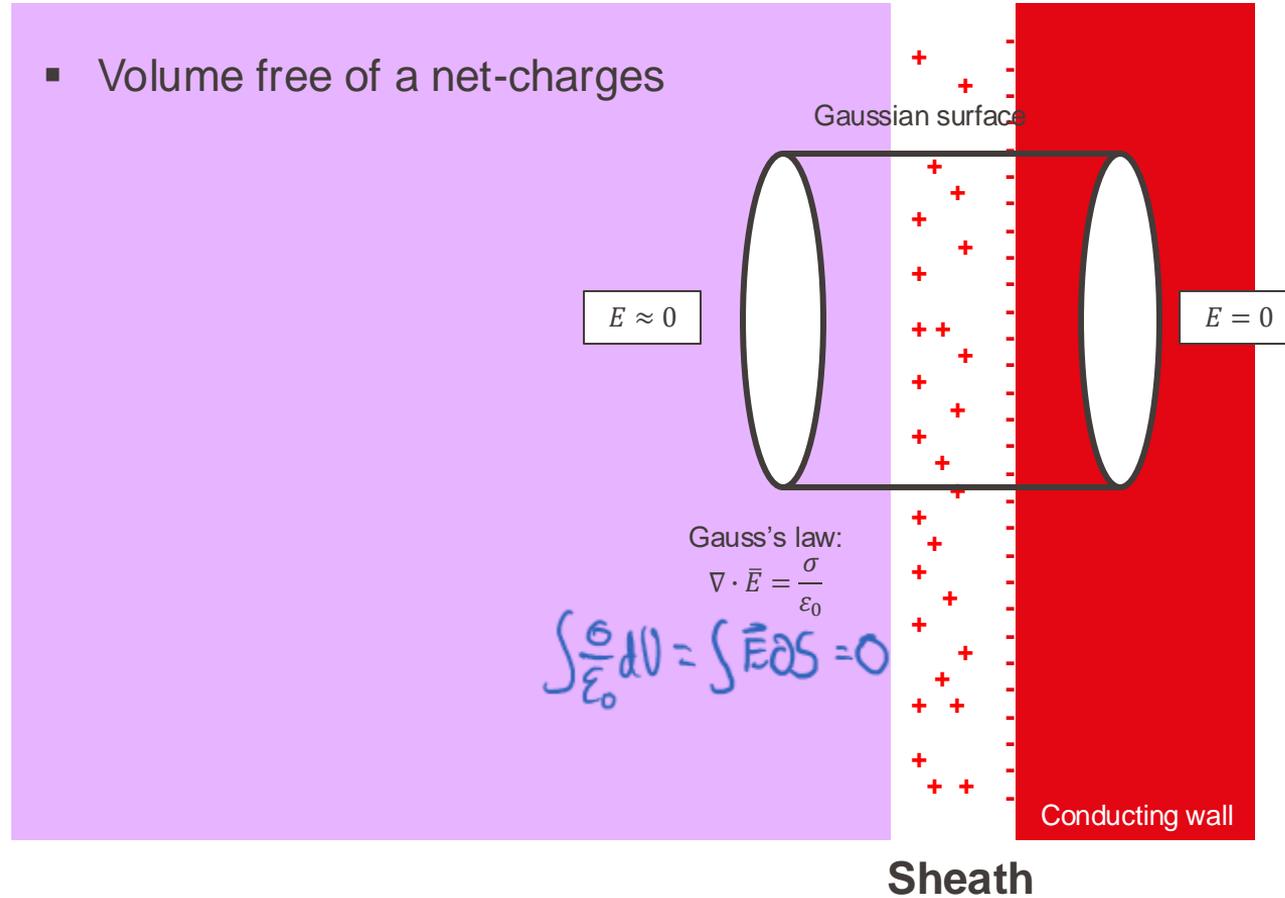
# Formation of a sheath

- Fast electrons rush to the wall, leaving behind a layer of slower ions
- Plasma potential increases until fluxes become equal
- Directional ion flux due to sheath electric field



# Formation of a sheath

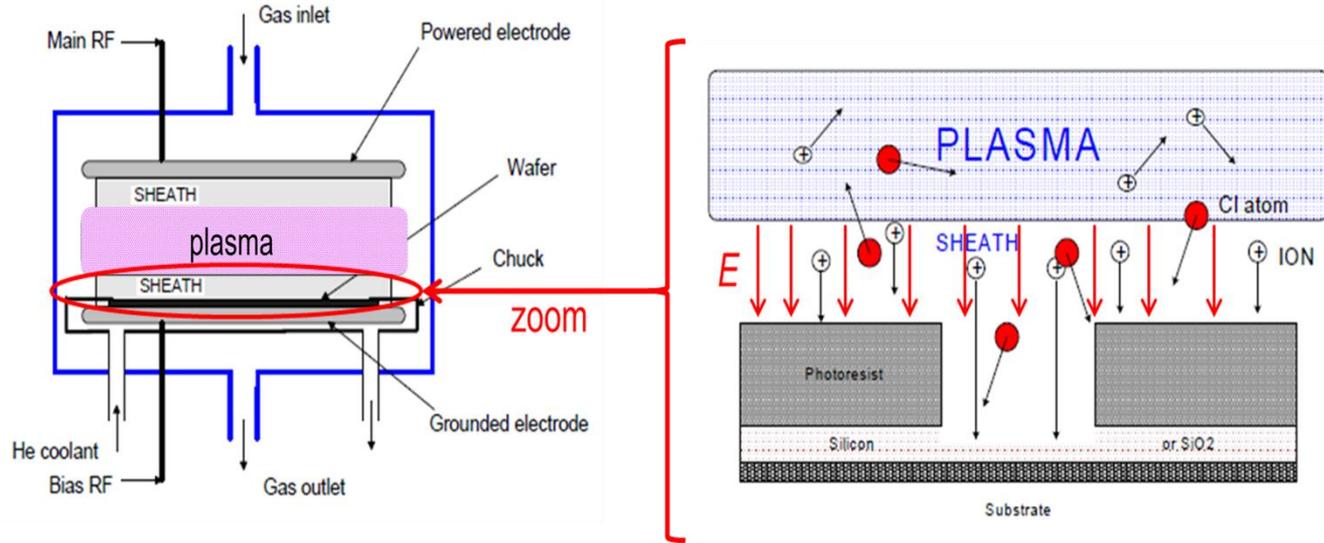
- Volume free of a net-charges



# Some sheath properties

- Sheath provides transition between plasma and wall
- Positive space charge equal and opposite to negative surface charge
- Electric field guarantees ambipolar ion and electron fluxes to wall (floating)
  - Strong electric field and a positive ion flux, normal and directed towards the wall
- Plasma potential is always positive with respect to most positive surface
- Thin layer, several Debye lengths thick, due to Debye screening of sheath potential

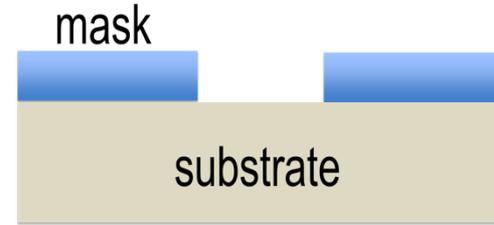
# Plasma etch applications



- Uniform electric field above a substrate
- Vertical flux of ions
- Photoresist feature  $\sim 0.1 \mu\text{m} \ll$  sheath width ( $\text{mm}$ )

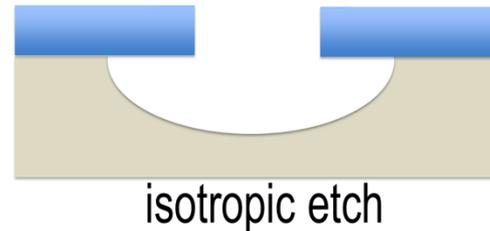
# Plasma etch applications

- Examples of high-aspect ratio etching



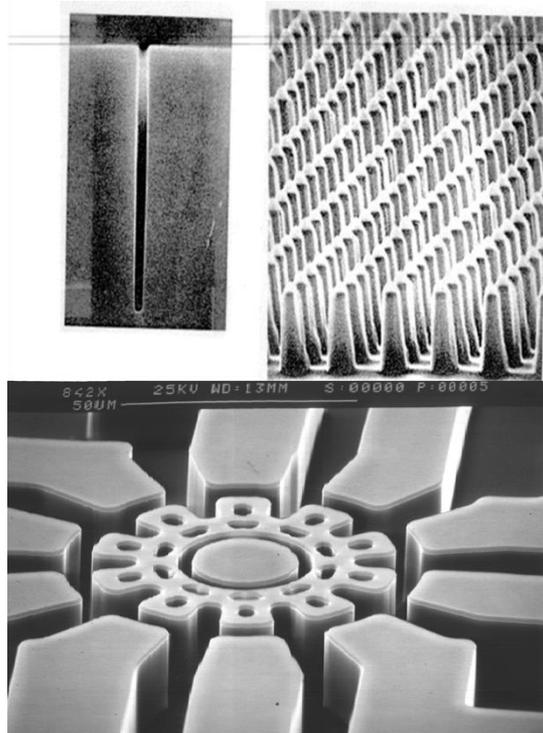
Chemical etching:  $A + \text{srfc}[C] \rightarrow AC$

wet process



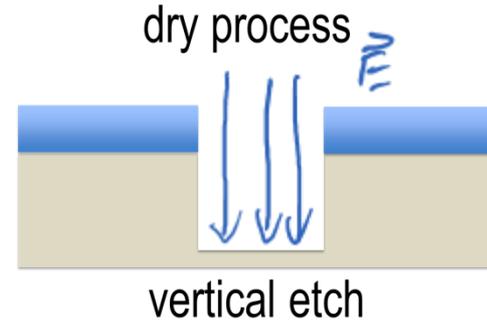
# Plasma etch applications (dry etching)

- Examples of high-aspect ratio etching



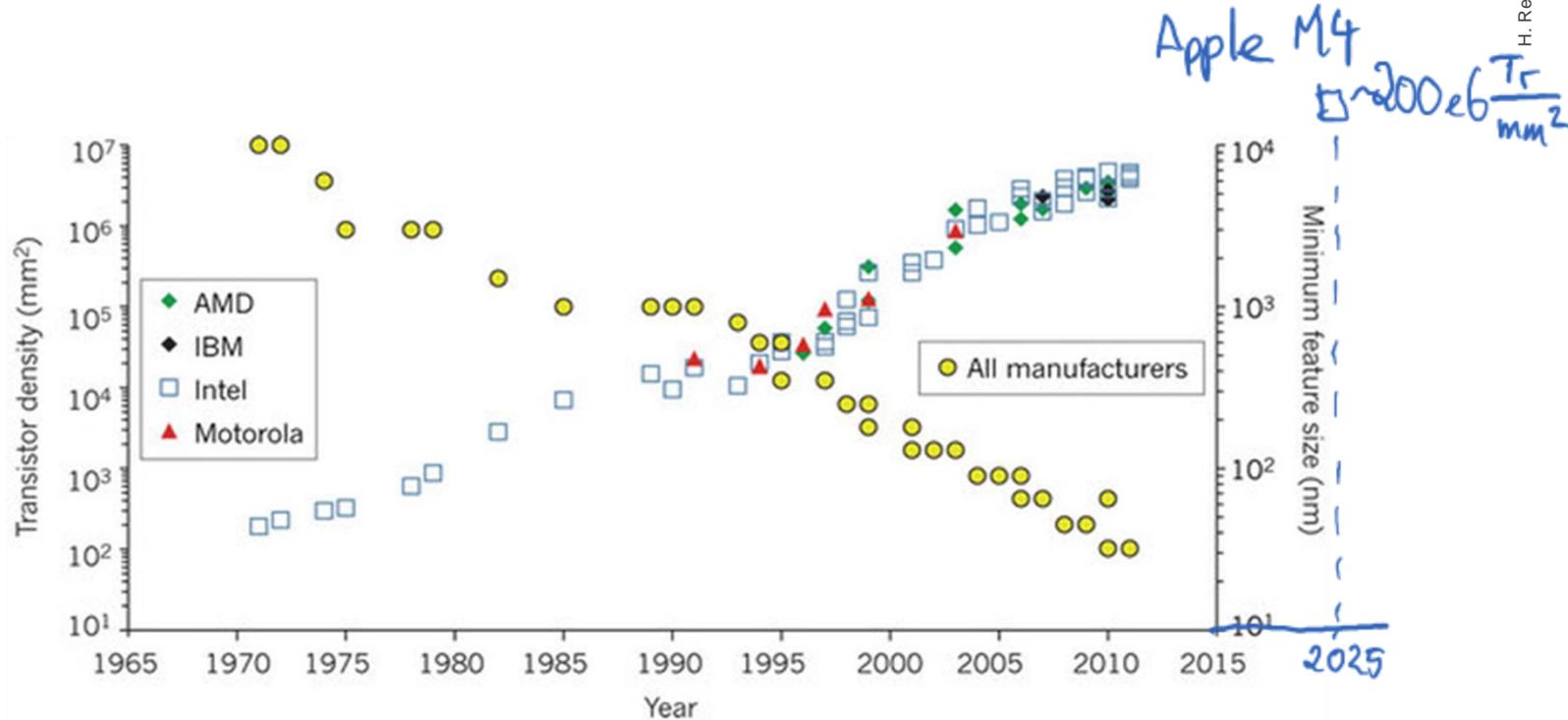
Reactive-ion etching:  $A^+ + \text{srfc}[C] \rightarrow AC$

- Directionality of ions crossing the sheath provides anisotropic etching



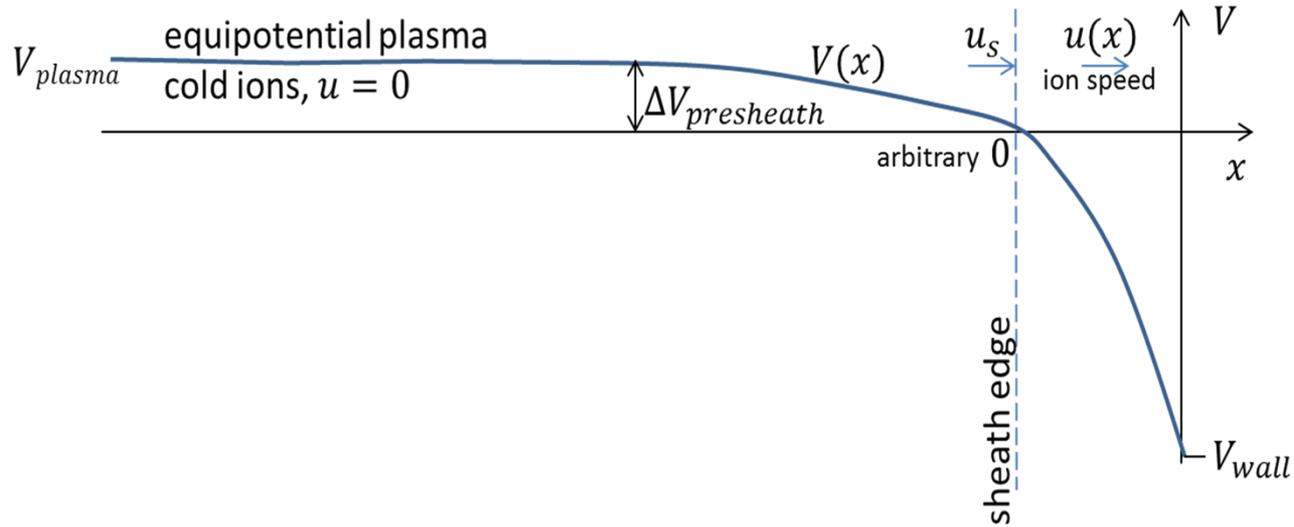
- Plasma processing is the only commercial technology capable of such control and indispensable for modern IC manufacturing!

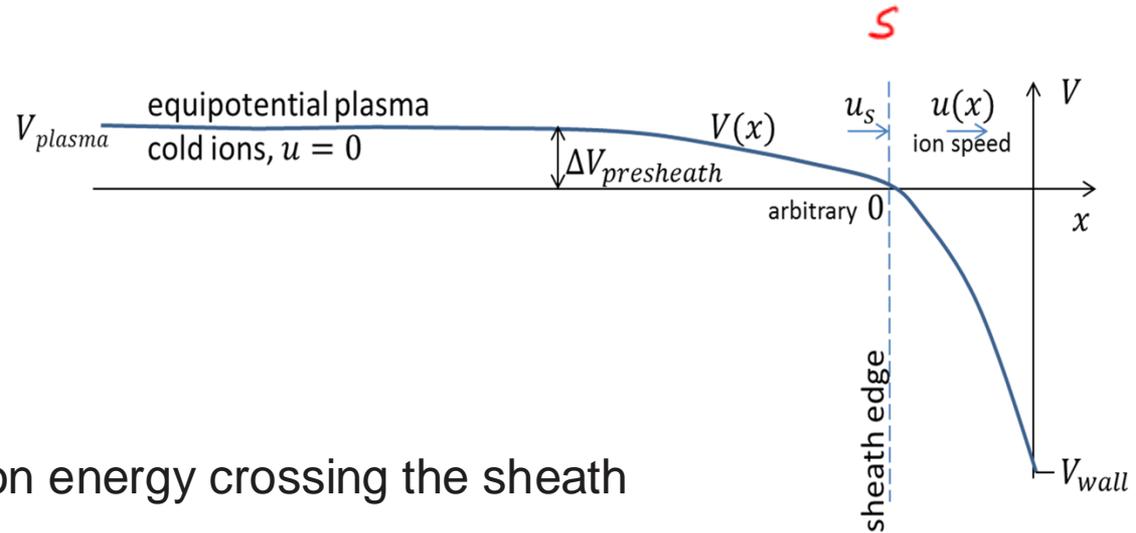
# Plasma etch applications



- First p-n junction transistor – Shockley, Sparks, Teal - ~1951
- Basis for integrated circuits invented by Kilby and Noyce
- Early integrated circuits (1961 Fairchild camera) had 25 - 40  $\mu m$  feature sizes
- Number of transistors per circuit doubles every couple of years (Moore's law, 1965)

# Sheath potential (qualitative)



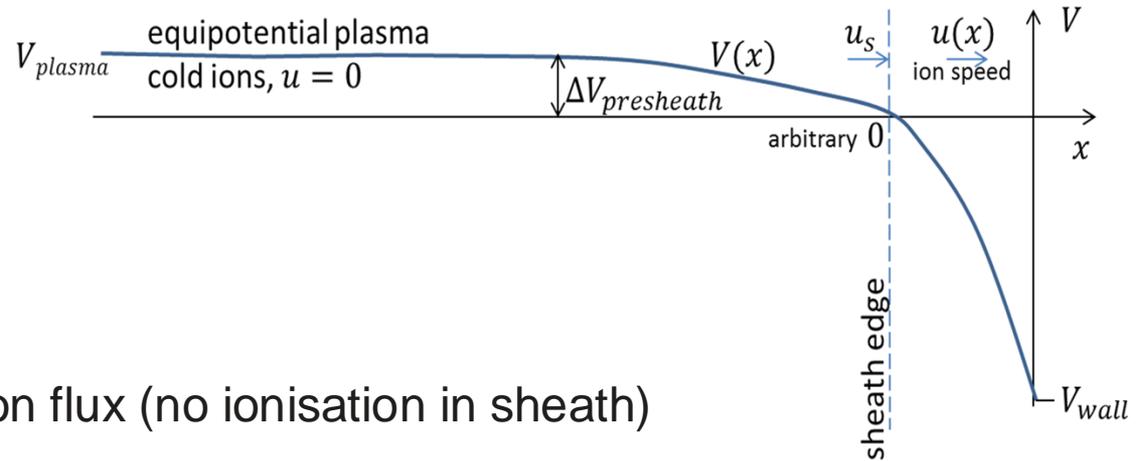


- Conservation of ion energy crossing the sheath (no collisions)

$$\frac{1}{2}Mu^2 + eV = \frac{1}{2}Mu_s^2$$

- Solve for  $u$

$$u(x) = \frac{2}{M} \left( \frac{1}{2}Mu_s^2 - eV \right)^{\frac{1}{2}} = \left( u_s^2 - \frac{2eV(x)}{M} \right)^{\frac{1}{2}} = u_s \left( 1 - \frac{2eV}{Mu_s^2} \right)^{\frac{1}{2}}$$



- Conservation of ion flux (no ionisation in sheath)

$$n_i u = n_s u_s$$

- Solve for  $n_i$

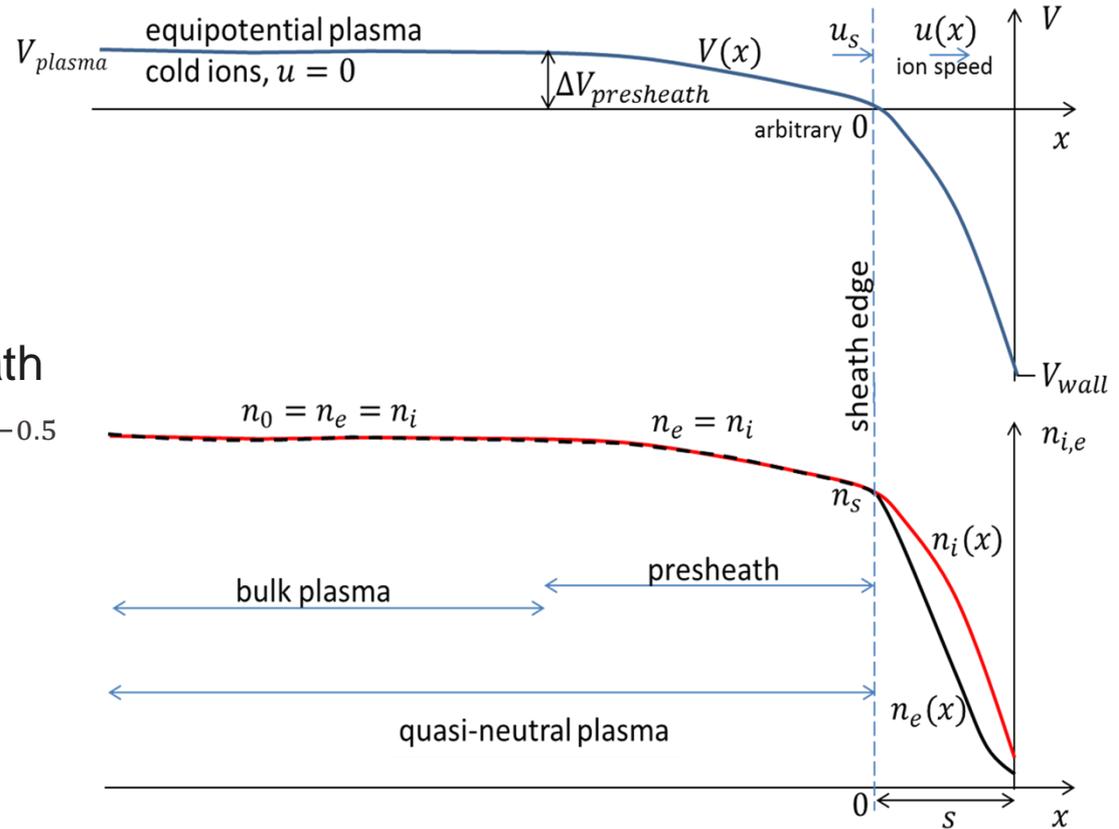
$$n_i(x) = \frac{n_s u_s}{u(x)} = \frac{n_s}{\sqrt{1 - \frac{2eV(x)}{M u_s^2}}}$$

- Ion density in sheath

$$n_i = n_s \left( 1 - \frac{2eV}{Mu_s^2} \right)^{-0.5}$$

- Electron density in sheath

$$n_e = n_s \exp\left(\frac{V}{T_e}\right)$$



- 1D Poisson's equation in sheath

$$\frac{d^2V}{dx^2} = -\frac{(n_i - n_e)e}{\epsilon_0}$$

Gauss's law  
 $\nabla \cdot \vec{E} = \frac{\sigma}{\epsilon_0}$

- Substitute charge densities (see previous page)

$$\frac{d^2V}{dx^2} = \frac{en_s}{\epsilon_0} \left[ \exp\left(\frac{V}{T_e}\right) - \left(1 - \frac{2eV}{Mu_s^2}\right)^{-0.5} \right]$$

- Taylor expand at the plasma-sheath interface

$$\frac{d^2V}{dx^2} = \frac{en_s}{\epsilon_0} \left[ \left(1 + \frac{V}{T_e}\right) - \left(1 + \frac{eV}{Mu_s^2}\right) \right] = \frac{en_s}{\epsilon_0} \underbrace{\left[ \frac{1}{T_e} - \frac{e}{Mu_s^2} \right]}_{\geq 0} V$$

- Require a physical, i.e. **non-oscillatory solution**  $\geq 0$

- The ion speed at the sheath entrance is  $u_s \geq u_B = \sqrt{\frac{eT_e}{M}}$

**Bohm's criterion**

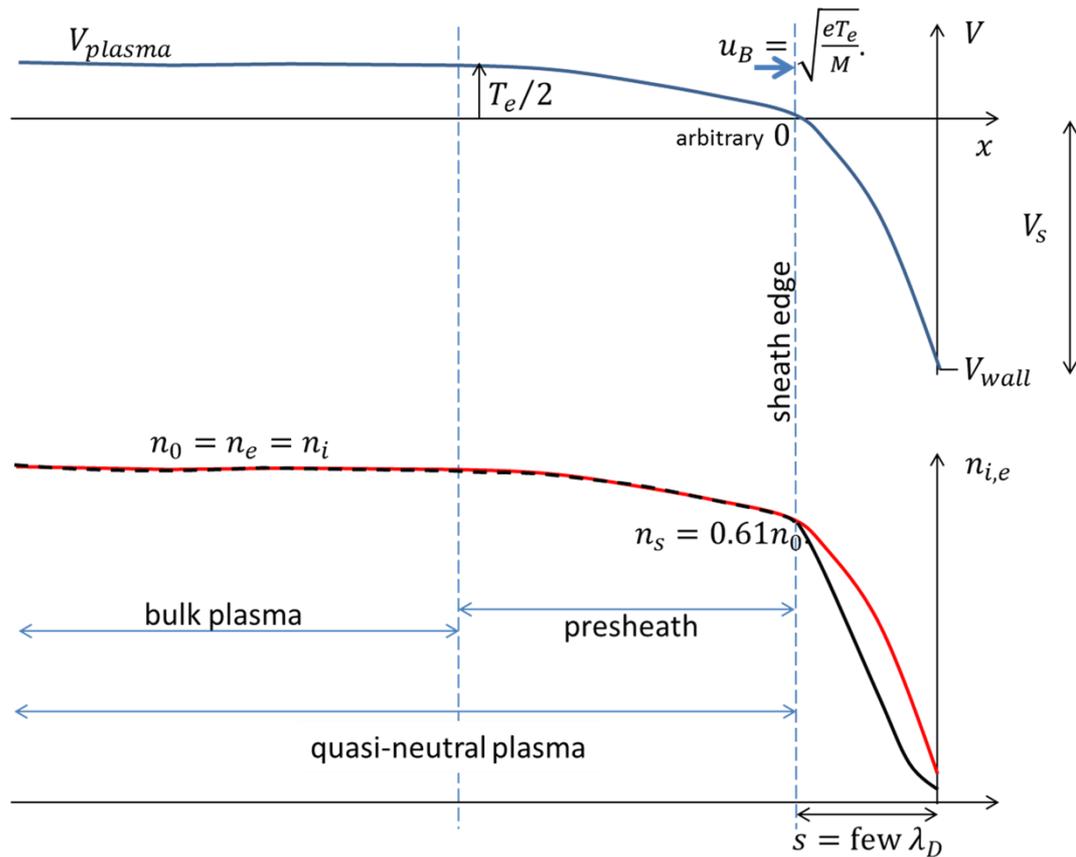
- Ion speed entering the sheath

$$u_s \geq u_B = \sqrt{\frac{eT_e}{M}}$$

- The ion velocity depends on the electron temperature
- The ions are accelerated to an energy  $\frac{1}{2}Mu_B^2 = eT_e/2$  in the presheath  
→ the presheath potential drop is  $V_{\text{presheath}} = T_e/2$
- The electron, hence, plasma density at the sheath edge is

$$n_s = n_0 \exp(-V_{\text{presheath}}/T_e) = n_0 e^{-0.5} = 0.61n_0$$

# Re-visit potential and density profiles



# Bohm's consequence #1: ion flux and etch rate

- Bohm's criterion  $u_B = \sqrt{\frac{eT_e}{M}}$  applies in all cases since the maximum potential drop in the pre-sheath cannot be  $\gg T_e/2$  (Debye screening)

- Collision-less sheath: ion flux into sheath = ion flux to the wall

$$\Gamma_i = n_s u_B = n_s \sqrt{\frac{eT_e}{M}} \approx 0.61 n_0 \sqrt{\frac{eT_e}{M}}$$

- If the wall is electrical floating, there is no current to the wall:  $\Gamma_i = \Gamma_e$

- The ion flux controls the etch rate  $\rightarrow$  plasma density & electron temperature

- Equally applies for a negatively biased wall  $j_{\text{sat}} = e\Gamma_i$

# Bohm's consequence #2: ion bombardment energy

- For a floating wall

$$\Gamma_i = n_s u_B \stackrel{!}{=} \Gamma_e = \frac{\bar{v}_e}{4} n_{e,\text{wall}} = \frac{\bar{v}_e}{4} n_s \exp\left(\frac{V_{\text{wall}}}{T_e}\right) = \frac{1}{4} \sqrt{\frac{8eT_e}{\pi m_e}} n_s \exp\left(\frac{V_{\text{wall}}}{T_e}\right)$$

$$\sqrt{eT_e/M}$$

➤ Potential drop in the sheath  $V_s = -V_{\text{wall}} = \frac{T_e}{2} \ln\left(\frac{M}{2\pi m_e}\right)$

- Total ion energy

$$\begin{aligned} \varepsilon_i &= e(V_{\text{plasma}} - V_{\text{wall}}) = e(V_{\text{pre-sheath}} + V_s) \\ &= e\left[\frac{T_e}{2} + \frac{T_e}{2} \ln\left(\frac{M}{2\pi m_e}\right)\right] \approx \frac{eT_e}{2} \ln\left(\frac{M}{2.3m_e}\right) \end{aligned}$$

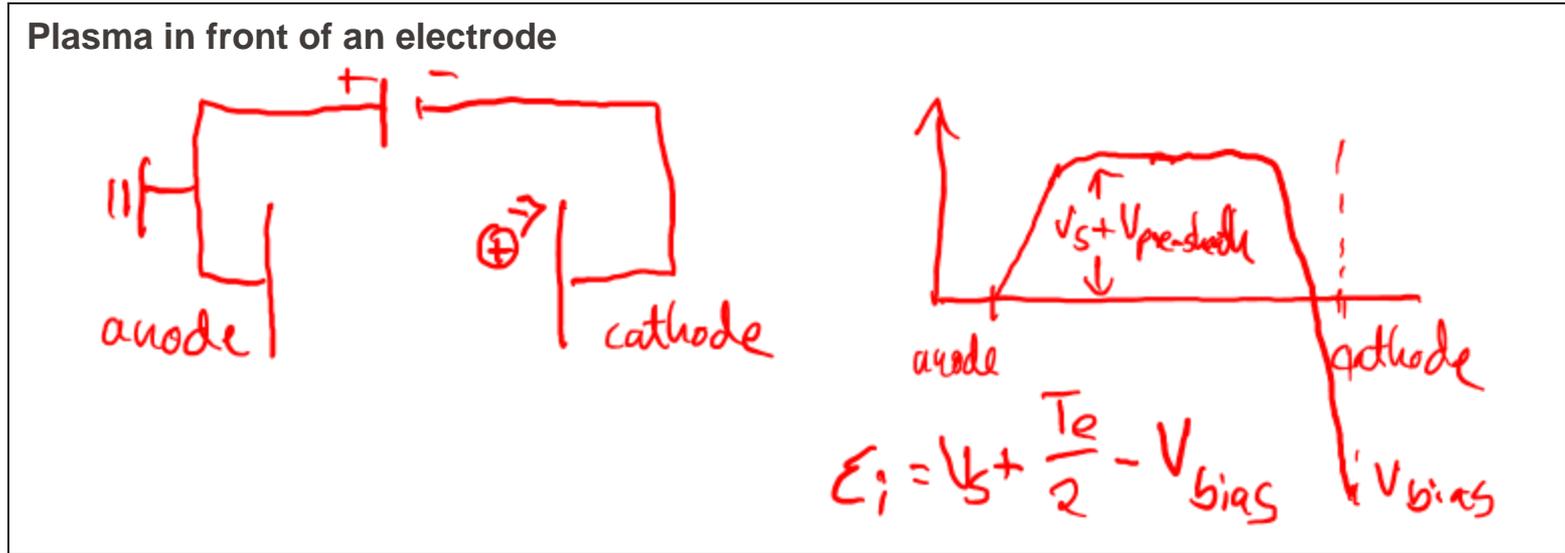
Ex.: Ar  $M=40$   
 $V_s = 4.7eT_e$   
 $\varepsilon_i = 5.2eT_e$

is controlled by ion mass and electron temperature

- Can be increased by biasing!

# Bohm's consequence #2: ion bombardment energy

- Increase ion energy by a negative bias of the wall ( $\rightarrow$  electrode)



- Bias drives a current up to  $j_{sat}$

# Summary of sheaths and plasma etching

- Sheath formation due to fact that  
electron mobility  $\gg$  ion mobility
- Deduce basic properties of a sheath
- Directional ions in plasma etching indispensable for IC manufacturing
- Bohm velocity for ions into a sheath

$$u_B = \sqrt{\frac{eT_e}{M}}$$

- Ion flux to a wall (controls etch rate)

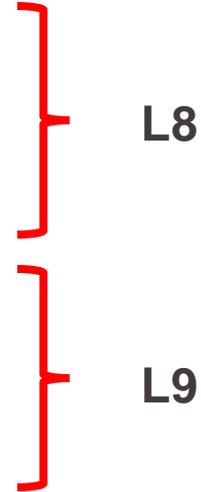
$$\Gamma_i = 0.61n_0\sqrt{\frac{eT_e}{M}}$$

- Ion energy to a wall

$$\varepsilon_i = \frac{eT_e}{2} \ln\left(\frac{M}{2.3m_e}\right) \sim 5.2eT_e$$

# Outline – Industrial plasmas

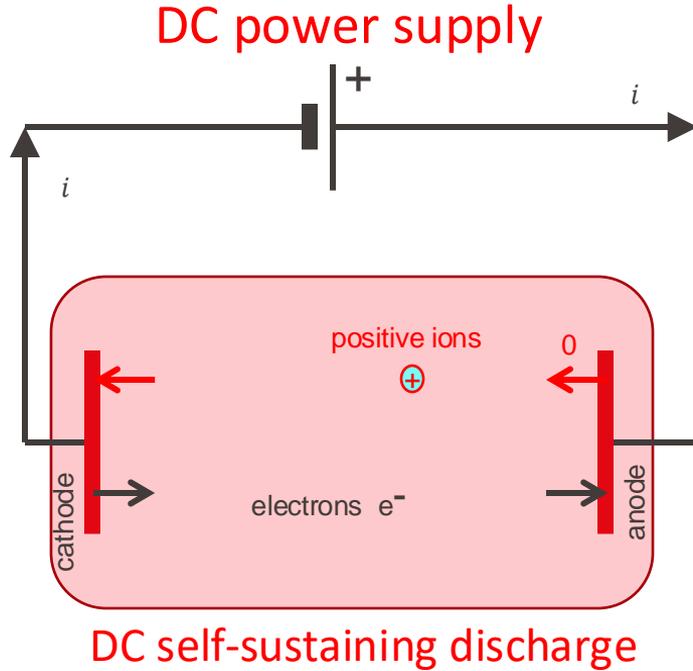
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2. Breakdown and Paschen's law
  - Communication satellite
3. Sheath and plasma etching
  - Microelectronics
4. **Plasma with insulating electrodes**
  - **RF – radio frequency, large area for solar cells**



## Material

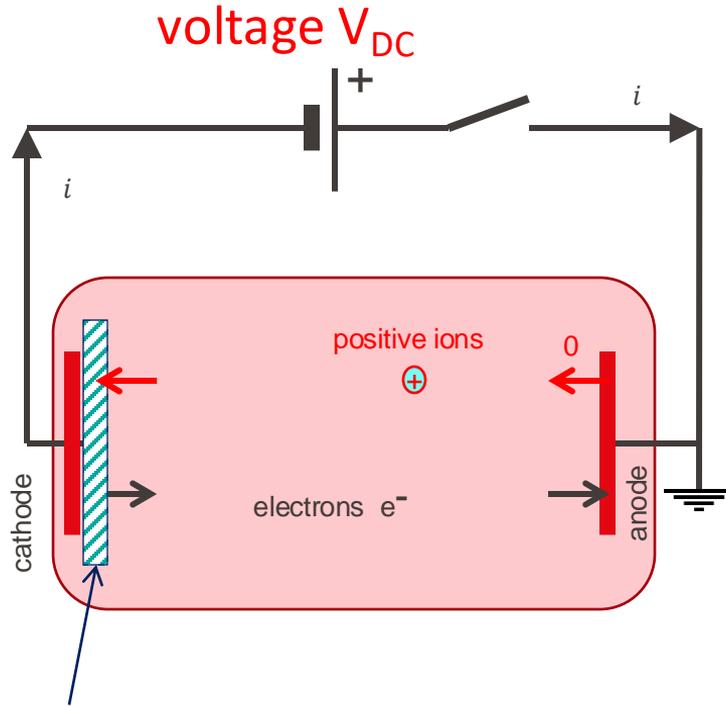
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# Can we use DC (Direct Current) for all plasma processing?

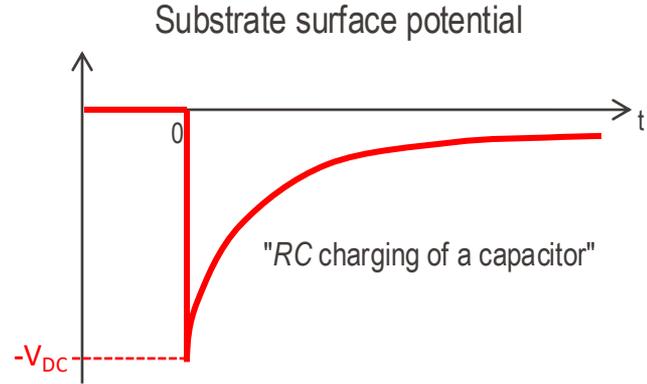


- The current everywhere is a **conduction current** due to moving charges
  - Electrons in the external circuit
  - Free ions and electrons in the plasma

# Consider an insulating layer on an electrode

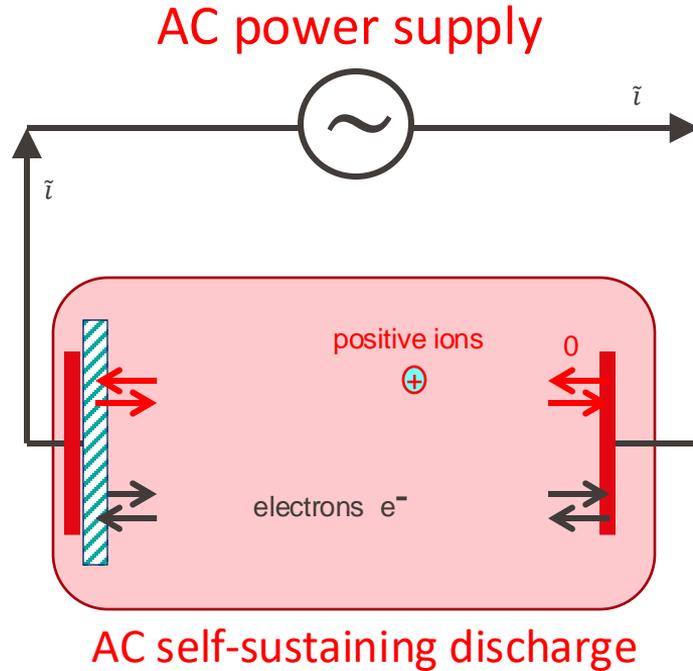


glass substrate, or an insulating film (SiO<sub>x</sub>), etc.  
This is a **dielectric** barrier



- Close the switch at time *t*=0
  - Plasma breaks down
  - Ions arrive at the glass surface
  - The insulating surface charges up
  - The surface voltage rises
  - The discharge voltage falls
  - The E-field is too low for ionization
  - The discharge current falls to zero

# Need to use AC (Alternating Current) for continuous plasma processing



- An insulating surface is alternately charged up, then *discharged* by the opposite field direction

- Typical plasma density  $\sim 5 \cdot 10^{16} \text{m}^{-3}$
- Ion plasma frequency

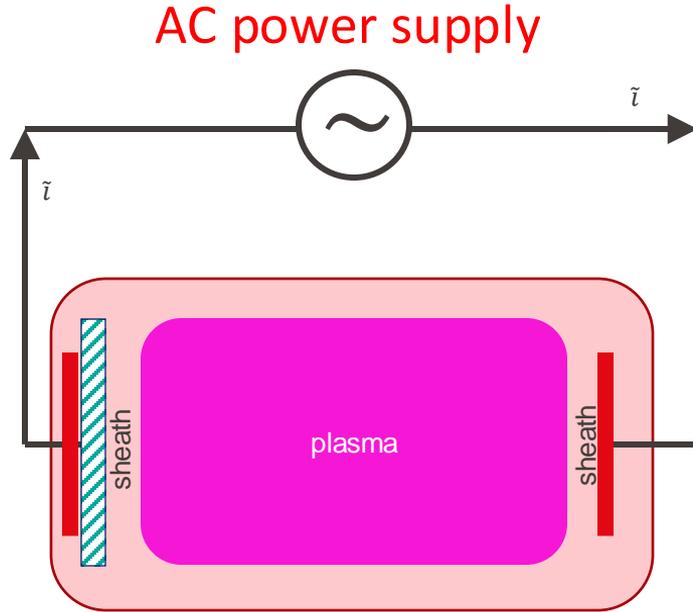
$$\frac{1}{2\pi} \sqrt{\frac{ne^2}{\epsilon_0 M}} \sim 2 \text{ MHz}$$

- Electron plasma frequency

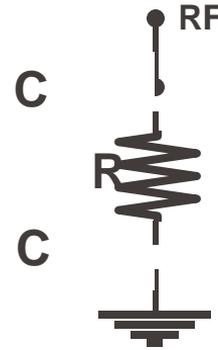
$$\frac{1}{2\pi} \sqrt{\frac{ne^2}{\epsilon_0 m_e}} \sim 500 \text{ MHz}$$

- At the industrial (ISM) frequency **13.56 MHz**
  - Electrons can follow the  $E$ -field
  - Ions only see the time-averaged  $E$ -field

# RF (radio-frequency) capacitively-coupled plasma for plasma processing

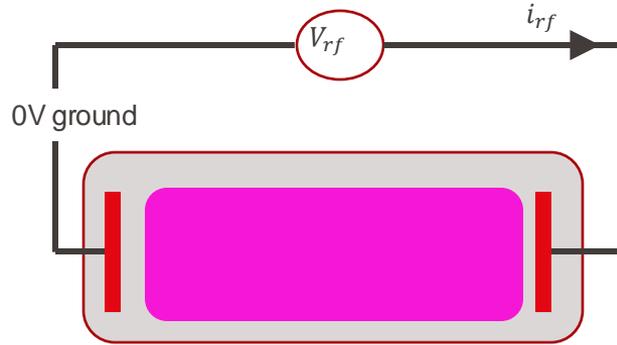


Simplified equivalent circuit for plasma

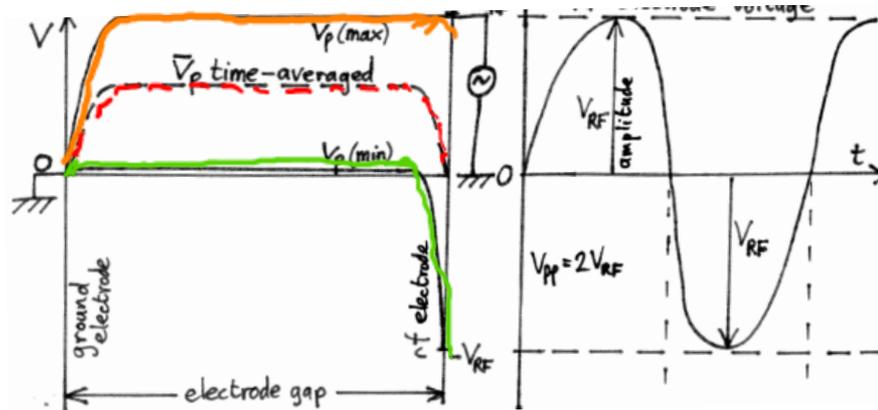


- RF current in circuit and plasma is a **conduction current** (moving charges)
- RF current in sheaths and the dielectric is a **displacement current**

# Basics of radio-frequency plasma



- Plasma potential always positive with respect to most positive surface



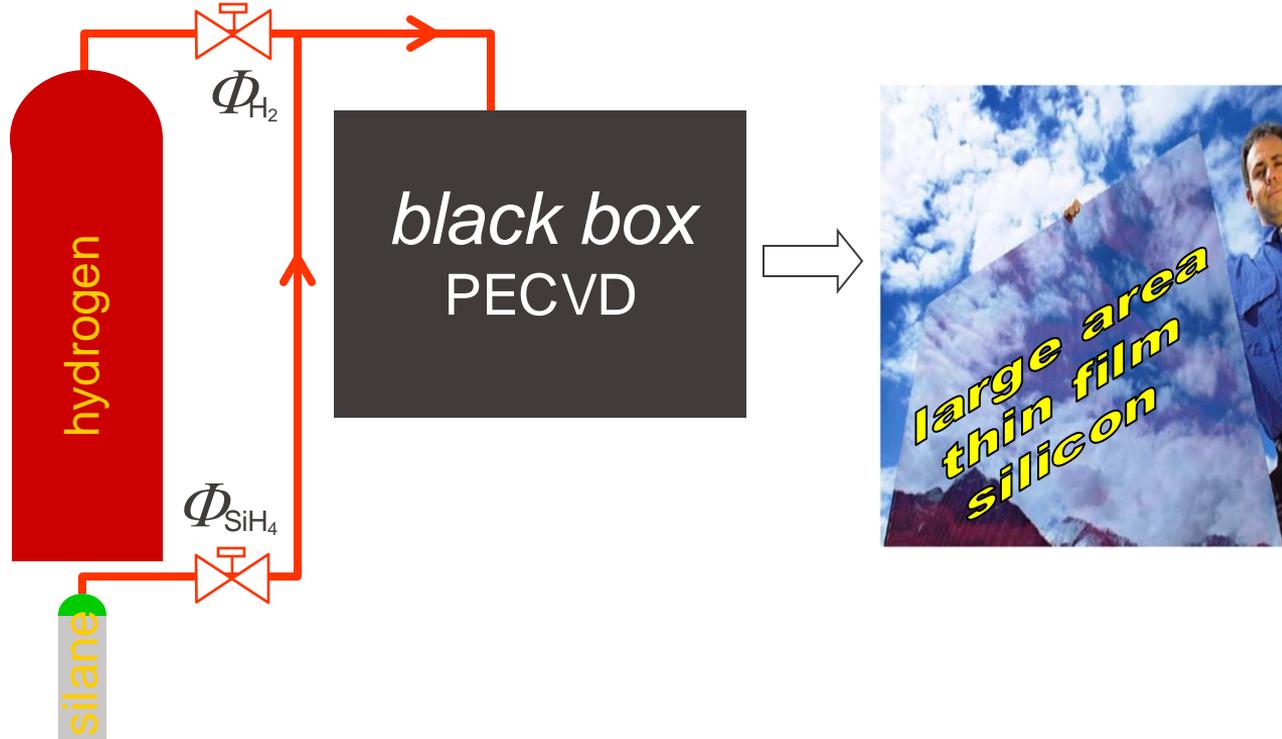
- Time-averaged sheath voltage  
 $= \text{RF amplitude}/2$   
 $= V_{p-p}/4$

➤ Method to chose ion energy  $\varepsilon_i \sim V_{pp}/4 \rightarrow$  useful for etch control

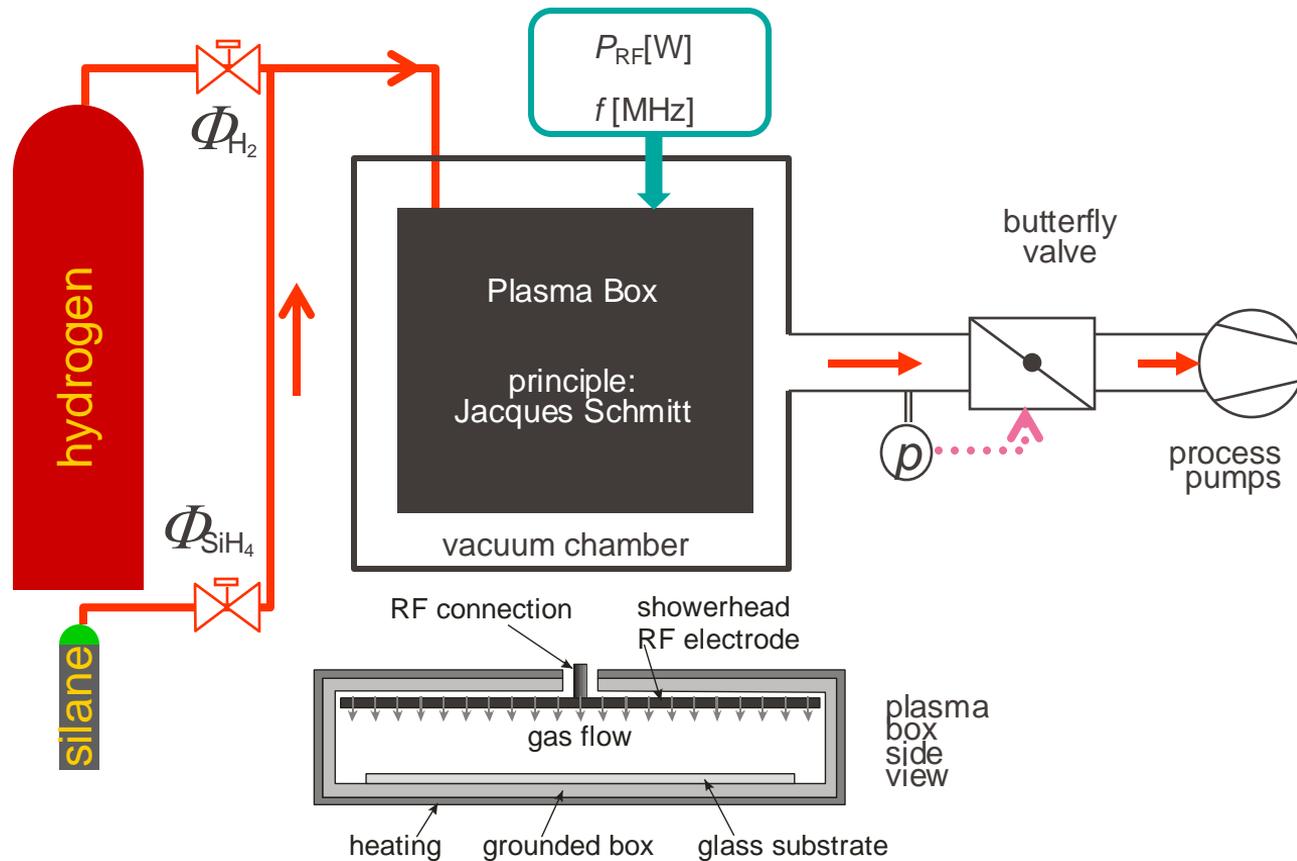
# Large area RF capacitively-coupled reactors

- Concentrate on plasma processing for large area electronics
  - Thin film transistors for flat panel LCD displays
  - Photovoltaic solar panels
- Swiss industries (historic)
  - Balzers displays
  - Unaxis Displays
  - Unaxis Solar
  - Oerlikon Solar/TEL Solar

# Plasma-Enhanced Chemical Vapour Deposition (PECVD) of thin film silicon



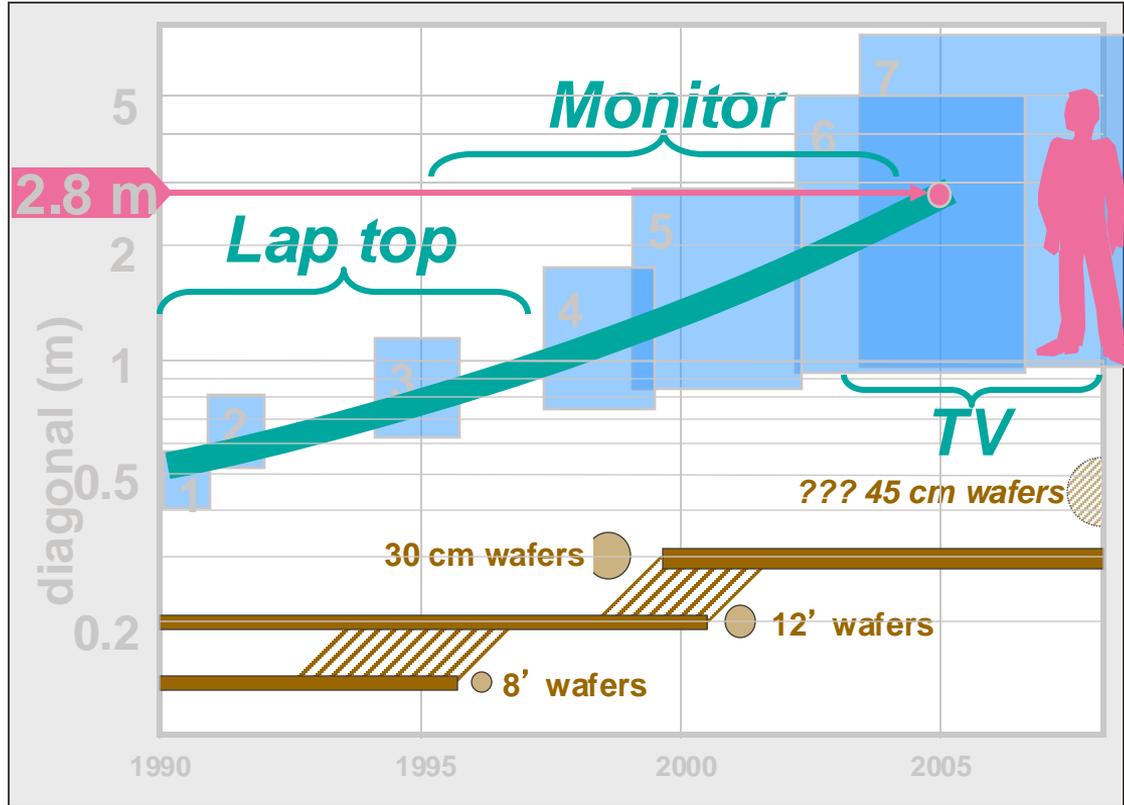
# PECVD capacitive, parallel-plate RF reactor - some typical specificities



## Front and back View Photo of KAI 20-1200



# Substrate size trend



# Summary of plasma with insulating electrodes

## RF capacitively-coupled plasma

- Conduction current in plasma, displacement current in sheaths/dielectric
- Industrial frequency 13.56MHz between ion and electron plasma frequency
- Sheath voltage and ion energy  $V_{p-p}/4$
- Large area, RF capacitively-coupled plasmas for solar cells

# Dielectric Barrier Discharge (DBD) for the production of Ozone O<sub>3</sub>

- Ozone is a powerful oxidizing agent, far stronger than O<sub>2</sub> (used for sterilization of water on industrial scale)
- Ozone can be used for combustion reactions and combusting gases
  - Provides higher temperatures than combusting in O<sub>2</sub>
- Ozone has a half-life of approximately a day at room temperature

# Ozone production by plasma chemistry

1. Plasma dissociation of oxygen

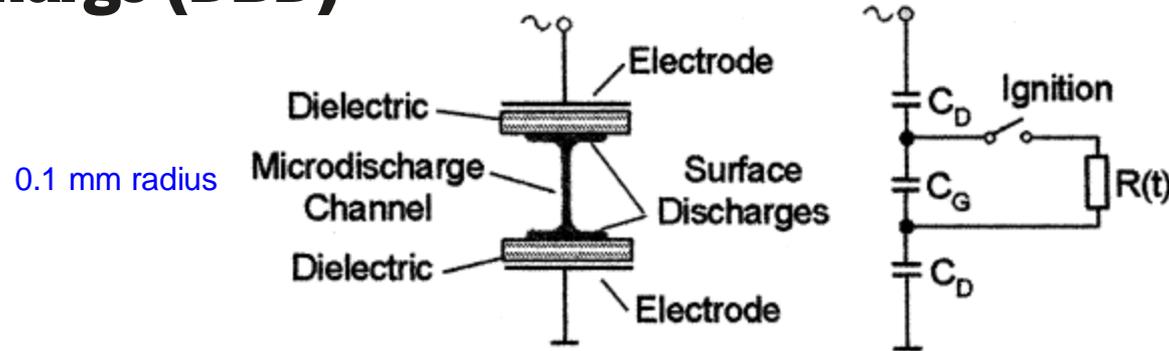


2. Ozon production by 3-body recombination



with  $M$  being any third body to carry of excess energy

# Ozon production by Dielectric Barrier Discharge (DBD)



- High voltage  $10^2 - 10^4 V$  causes local breakdown between the electrodes at atmospheric pressure ( $10^{14} - 10^{15}$  electrons/ $cm^3$ )
- A filamentary discharge occurs at this position with avalanche flow of electrons (streamer)  $100 - 1000 A/cm^2$
- Dielectric surface charges up ( $100 pC$ ) and local voltage is reduced in  $ns$
- Arc extinguishes, but neighbouring arc can still strike
- High voltage alternates at  $50 Hz$  to  $100 MHz$
- The dielectric
  - 1) limits energy of individual discharges ( $mJ$ )
  - 2) distributes the arcs over the entire area

# Photograph of DBD arcs through a transparent electrode

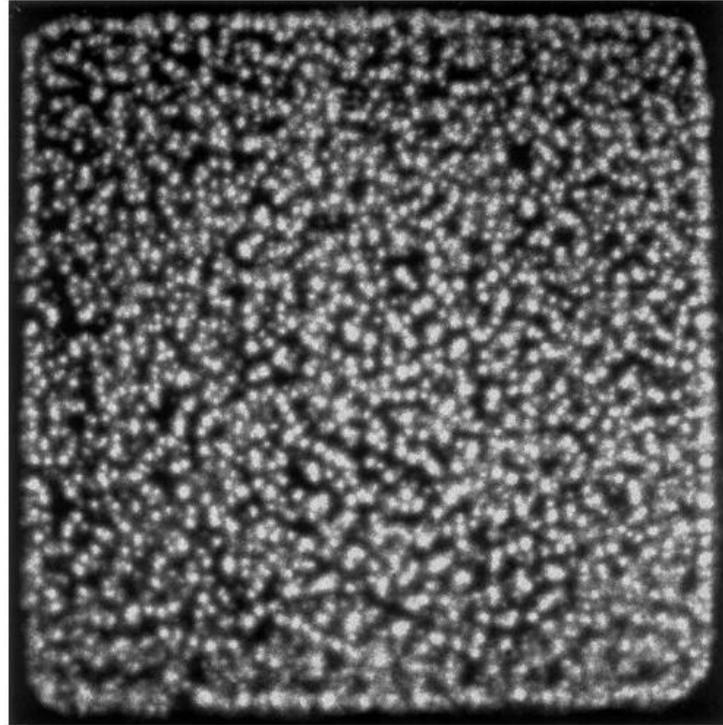


Fig. 3. End-on view of microdischarges in atmospheric-pressure air (original size: 6 cm × 6 cm, exposure time: 20 ms).

# Summary of plasma with insulating electrodes

## RF capacitively-coupled plasma

- Conduction current in plasma, displacement current in sheaths/dielectric
- Industrial frequency 13.56MHz between ion and electron plasma frequency
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## Dielectric Barrier Discharge

- Transient (*ns*), filamentary arcs, atmospheric pressure
- DBD Ozon generation for water purification

# Reminder: Maxwell-Boltzmann distribution

- Velocity distribution in an ideal gas in thermodynamic equilibrium

$$f_s(v) = \left( \frac{m_s}{2\pi k_B T_s} \right)^{3/2} e^{-\frac{m_s v^2}{2k_B T_s}}$$

- Most probable velocity:

$$v_{p,s} = \sqrt{\frac{2k_B T_s}{m_s}}$$

- Mean velocity:

$$\bar{v}_s = \sqrt{\frac{8k_B T_s}{\pi m_s}}$$

- Root-mean-square velocity:

$$v_{\text{rms},s} = \sqrt{\frac{3k_B T_s}{m_s}}$$